

Low-Pass Filter Design Example

- Design a Low-Pass Filter with cut-off frequency of 900 MHz and a stop band attenuation of 18 dB @ 1.8 GHz.
- From the Butterworth Nomograph, $A_{max} = 1$ and $A_{min} = 18$. $A_{max} = 1$ since unity gain. And the order of the filter is $N = 3$.
- From Butterworth Tables, $g_1 = g_3 = 1.0$ and $g_2 = 2$.

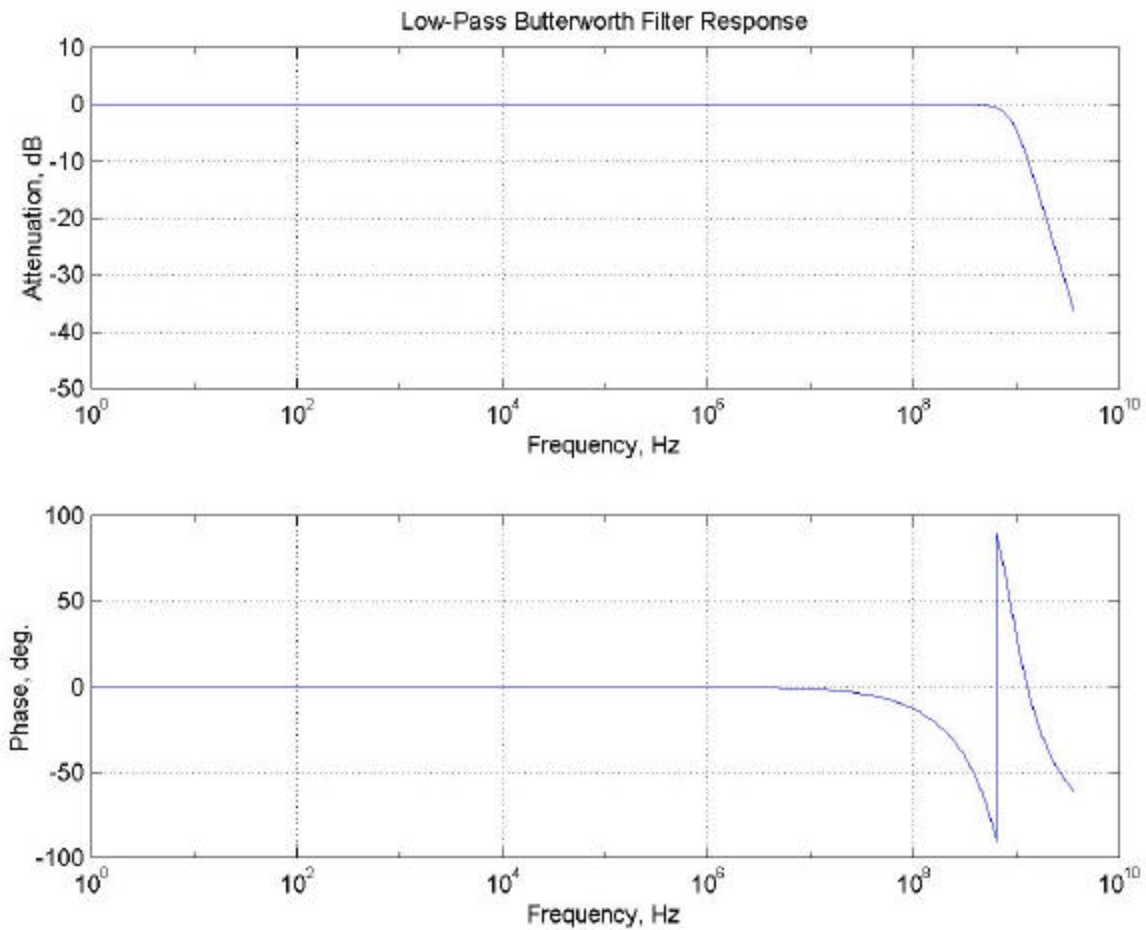
Low-Pass Filter Design Example

- De-Normalized Values For the Tee-Configuration Low-Pass Filter Are:

$$L_1 = L_2 = \frac{g_1 R_L}{2p (900 \times 10^6)} = 8.8 \text{ nH}$$

$$C_1 = \frac{g_2}{2p (900 \times 10^6) R_L} = 7 \text{ pF}$$

Low-Pass Filter Design Example



Low- To High-Pass Transformation

- Transform the Low-Pass Filter Normalized Component Values to the Normalized High-Pass Values
- Inductors in Low-Pass Configuration Become Capacitors in High-Pass.
- Capacitors in Low-Pass Configuration Become Inductors in High-Pass

- $$C_{HP_norm} = \frac{1}{\omega_c L_{LP_norm}} ; L_{HP_norm} = \frac{1}{\omega_c C_{LP_norm}}$$

RF Filter Parameters

- Insertion Loss: $IL = 10 \log \frac{P_{in}}{P_L} = -10 \log (1 - |\Gamma_{in}|^2)$
- Ripple
- Bandwidth: $BW^{3dB} = f_u^{3dB} - f_L^{3dB}$
- Shape Factor: $SF = \frac{BW_{A_{min}}}{BW_{A_{max}}}$
- Rejection

De-Normalizing Filter Component Values

- All Normalized Component Values Are De-Normalized Using the Following:




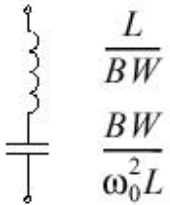
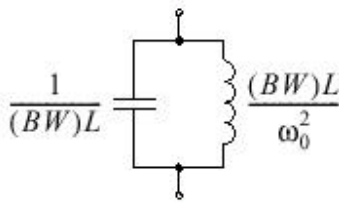
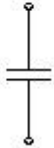


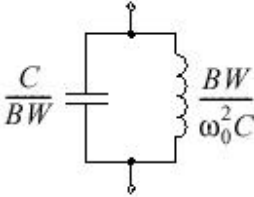
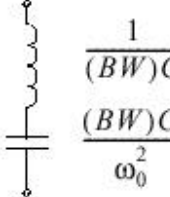
$$C_{actual} = \frac{C_{normalized}}{R_g}$$

and

$$L_{actual} = L_{normalized} R_g$$

Transformation From Low-Pass Filter

Table 5-5 Transformation between normalized low-pass filter and actual bandpass and bandstop filter
 $(BW = \omega_U - \omega_L)$

Low-pass prototype	Low-pass	High-pass	Bandpass	Bandstop
 $L = g_k$	 $\frac{L}{\omega_c}$	 $\frac{1}{\omega_c L}$	 $\frac{L}{BW}$ $\frac{BW}{\omega_0^2 L}$	 $\frac{1}{(BW)L}$ $\frac{(BW)L}{\omega_0^2}$
 $C = g_k$	 $\frac{C}{\omega_c}$	 $\frac{1}{\omega_c C}$	 $\frac{C}{BW}$ $\frac{BW}{\omega_0^2 C}$	 $\frac{1}{(BW)C}$ $\frac{(BW)C}{\omega_0^2}$

Normalized Low- to Band-Pass Filter Transformation

- Normalized Band-Pass Shunt Elements from Shunt Low-Pass Capacitor:

$$L_{BP_norm_shunt} = \frac{\omega_{upper} - \omega_{lower}}{\omega_o^2 C_{LP_norm}}$$

$$C_{BP_norm_shunt} = \frac{C_{LP_norm}}{\omega_{upper} - \omega_{lower}}$$

Normalized Low- to Band-Pass Filter Transformation

- Normalized Band-Pass Series Elements from Series Low-Pass Inductor:

$$L_{BP_norm_series} = \frac{L_{LP_norm}}{\omega_{upper} - \omega_{lower}}$$

$$C_{BP_norm_series} = \frac{\omega_{upper} - \omega_{lower}}{\omega_o^2 L_{LP_norm}}$$

Normalized Low- to Band-Stop Filter Transformation

- Normalized Band-Stop Shunt Component Values from Low-Pass Shunt Capacitor:

$$L_{Stop_norm_shunt} = \frac{1}{\left(\omega_{upper} - \omega_{lower}\right) C_{LP_norm}}$$

$$C_{Stop_norm_shunt} = \frac{\left(\omega_{upper} - \omega_{lower}\right) C_{LP_norm}}{\omega_o^2}$$

Normalized Low- to Band-Stop Filter Transformation

- Normalized Band-Stop Series Component Values from Low-Pass Series Inductor:

$$L_{Stop_norm_series} = \frac{\left(\omega_{upper} - \omega_{lower}\right) L_{LP_norm}}{\omega_o^2}$$

$$C_{Stop_norm_series} = \frac{1}{\left(\omega_{upper} - \omega_{lower}\right) L_{LP_norm}}$$